

Advanced Synthesis Procedures Of Magnesium Aluminate Spinel- A Review

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Abstract- Magnesium aluminate ($MgAl_2O_4$) spinel (MAS) is a man-made material with good chemical, thermal, dielectric, mechanical, and optical properties. These characteristics made MAS an essential material for optically transparent windows, domes, and armours, as well as other applications for a variety of refractory purposes. The main reason for this is the high processing cost of dense MAS ceramics. Despite its high performance, it is only used in a few key applications. The use of alumina and magnesia prevents the formation of thick MAS bodies in a single-stage reaction. As a result, dense MAS bodies are created by firing in two stages. This is a time-consuming and costly operation. According to the available literature, the processing cost of dense MAS ceramics can be significantly lowered by carefully selecting initial raw materials, powder processing and densification settings, and understanding the underlying mechanisms. MAS formation and densification mechanisms. Because there is very less review article on the subject, an attempt has been made to construct this review article with a complete and comprehensive understanding of MAS. Synthesis, processing, and key applications of MAS, as well as its utility for a number of fresh and inventive uses that will emerge in the future.

Keywords- Spinel, Magnesium Aluminate and Synthesis etc.

I. INTRODUCTION

Magnesium chemical compound ($MgAl_2O_4$) mineral may be a refractory chemical compound material consisting of variety of fascinating properties like high freezing point ($2135^\circ C$), high resistance against chemical attack, and high mechanical strength each at temperature ($135-216$ MPa modulus of rupture) and elevated temperatures ($120-205$ MPa modulus of rupture at $1300^\circ C$). [1] Typical synthesis of $MgAl_2O_4$ mineral is predicated on solid-state reaction of metal and atomic number 13 bearing compounds at high temperatures ($1600^\circ C$). It is terribly tough to arrange reactive mineral powders (particle size of 0.5 mm) with this method.

So as to arrange $MgAl_2O_4$ mineral powders with high purity and high reactivity, numerous non-conventional techniques, like co-precipitation, sol-gel, spray-drying, spray transmutation, freezing, flame spray transmutation, [2], [3] and mechanical activation, [4]-[8] [9], [10] are already established. The reactivity of calcined powder powerfully depends on the oxidation temperature. [11] The upper oxidation temperature triggers agglomeration, grain growths. Therefore, the synthesis of metal corundum mineral was targeted to get pure material at the bottom to attain oxidation temperature. The oxidation temperature for formation of pure mineral has been observed to be $1100^\circ C$ by co-precipitation, [12] $1200^\circ C$ by freeze-drying [13] and on top of $1200^\circ C$ by heterogeneous sol-gel. Monolithic mineral will be synthesized at $900^\circ C$ exploitation mechano chemical methodology.

[14] Metal chemical compound ($MgAl_2O_4$) or Magnesium Aluminate Spinel (MAS) is an artificial material with solid crystal structure. It exhibits excellent chemical, thermal, dielectric, mechanical and optical properties. These properties created MAS an important material for optically clear windows, domes, armours and refractory applications in iron and steel industries. High process value of dense MAS ceramics has restricted and necessary usage in the industry. The amount growth (8%) is related to MAS part formation that doesn't enable getting dense MAS bodies in an exceedingly single-stage reaction sintering method. Hence, dense MAS bodies are created by following double stage firing method. It is observed from literature review that the process value of dense MAS mineral can be reduced to a significant amount by correct choice of precursors, powder processing method, and by understanding the mechanisms of MAS formation and compression.

Recently, metal chemical compound ($MgAl_2O_4$) mineral is receiving an overwhelming attention from research world as well as the business sector on account of its many necessary properties like high melting point ($2135^\circ C$), high hardness (16GPa), comparatively low density (3.58 g/cm^3), high mechanical strength each at room (135–216 MPa) and elevated temperatures (120–205 MPa at $1300^\circ C$), high resistance against chemical attack, wide energy band gap, high electrical phenomenon, comparatively low thermal growth constant ($9 \times 10^{-6}/^\circ C$ between $300^\circ C$ and $1400^\circ C$), high thermal shock resistance, etc.[15]–[17]. Moreover, MAS doesn't react with SiO_2 till $1735^\circ C$, with MgO or CaO till $2000^\circ C$, with Al_2O_3 till $1925^\circ C$. Absolutely dense crystalline MAS is optically clear, likewise as within the millimeter IR regions, given the grain size is far but the wavelength of incident light weight.

Because it permits larger wall thickness than corundum while not losing its transparent properties, it is been used for optical engineering applications, like armoured window system, high energy optical mass windows and light-weight armour in defense industry. Now, MAS has replaced the normal corundum, sapphire, aluminium oxynitride (AlON), zinc sulfide (ZnS) ceramics in applications requiring lightweight transmission within the wavelength range of 2.5–5 μm . Resistance to radiation induced swelling and strength degradation created MAS a possible reactor power core insulator. As a result of

its basic nature, porous MAS each in bulk and skinny film type of characteristics showed its potential as an electronic sensing element.

It has low material constant and low loss tangent properties and because of its bonding with lattice structure with silicon and with variety of different necessary chemical compound systems, created MAS a beautiful material for integrated electronic devices. Considering its high melting point and high chemical immobility, MAS has been used to exchange ancient mineral based refractories in cement rotary kilns and steel ladles, since the refractories of latter generations contain chromium species, that produce each environmental and health hazards. Skinny films of MAS exhibited a good result in potential utility in limit coatings or thermal barrier coating (TBCs) for the blades and vanes within the hot section parts of gas turbines. Moreover, MAS has been used as another material to replace the traditional carbon anode in metallic element electrolytic cells. Its low acidity and thermal stability created MAS a very good catalyst for chemical reaction of ions SO_2 to SO_3 in the fields of environmental fossil oil process and fine chemical production.

Because of the on top of mentioned properties, MAS was potentially utilized as a catalyst support for an excellent type of reactions as well as De-SO_x, selective chemical process reduction (SCR) of NO, ammonia synthesis, n-butane dehydrogenation, dry reforming of paraffin, chemical process combustion (CPC), and water-gas shift reaction, chemical process steam reforming of paraffin and gas dehydrogenation. Although, an excellent variety of papers modify MAS within the literature, none of them offer along the entire information concerning the basics (properties, crystal structure and section diagram), the issues of volume enlargement related to MAS section formation from aluminum oxide and periclase, the effectiveness of single or double stage sintering processes, the ways available to scale back the process value of MAS product, the various routes used for the preparation of MAS powders, single crystals, whiskers and skinny films, the obtainable powder co-ordination (i.e. processing) techniques, chemical composition (i.e. non-stoichiometry), defect reactions, impurities/sintering aids, process routes, etc., on conglomerate behavior of the powder, the advanced spectral characteristics of the powders, the optical, mechanical, dielectric, magnetic

and thermal properties of mould materials, the applications, etc. This critique is an exertion to fill this diversion.

Synthesis routes of magnesium aluminate spinel (MAS)

1. Solid state reaction

Since it is difficult of getting MAS from nature, MAS is synthesized unnaturally or artificially. There are many chemical routes like co-precipitation, spray drying, freeze drying and spray shift which is used to synthesize MAS at very low temperatures. However, none of those processes is appropriate for producing of MAS in bulk amount for applications like refractories. Thus, solid compound sintering is a possible route for producing of MAS counts for refractory applications. The leading widespread methodology in industrial production is that the typical solid-state reaction of Mg and Al bearing precursors, like oxides, carbonates and hydroxides. The formation of MAS from compound of magnesium oxide and mineral is related to a volume enlargement, which may be simply predicted from their density variations (MgO: 3.58 g/cm², Al₂O₃: 3.99 g/cm², MgAl₂O₄: 3.58 g/cm²). This enlargement is analogous to a linear enlargement of 2.6% indicated to this volume enlargement.

Normally, double stage firing method is utilized to generate dense MAS grains for refractory applications. Considering two consecutive firing cycles, the price of MAS grain has been increased by a large or excessive amount. Lots of studies are devoted to understand the quantity enlargement behavior of MAS part formation and to scale back the process value of dense MAS grains for refractory applications. The linear thermal enlargement behaviour of various MgO/Al₂O₃ powder combinations compacts with sintering temperature was studied, and enlargement of compositions higher than 900°C was observed, which was attributed to the creation of the MAS portion.

However, due of the sintering temperature, some shrinkage was seen at temperatures higher than 1300°C. The MAS composition showed the greatest linear expansion (5%). The problem of obtaining dense MAS ceramics in a single-stage reaction sintering process is reflected in such an enlarged enlargement. Aside from that, MAS has a substantial solution variation on aluminium oxide at high

temperatures. With the solid solubility of aluminium oxide, the molar volume of MAS falls somewhat. MgAl₂O₄ has a theoretical value of 39.77 cm³.mol⁻¹, while MgO·₂Al₂O₃ has a theoretical value of 39.24 cm³.mol⁻¹. The composition at the boundary associated with Al₂O₃ at 1600°C is the latter. It is stated that the reaction takes place via counter diffusion of the cations, where chemical element ions stay at the starting locations, in the production of MAS portion from mineral and magnesium oxide during a solid-state reaction at extreme temperatures. 3Mg²⁺ diffuses toward the alumina side and 2Al³⁺ diffuses toward the magnesia side to establish electrical neutrality.

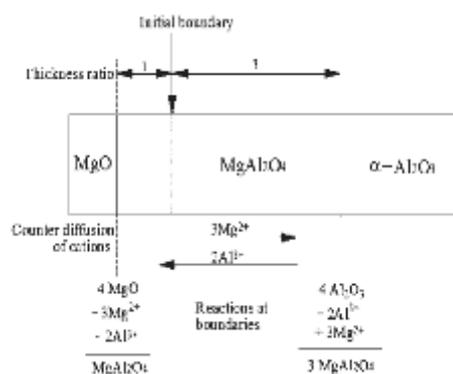


Figure 1 Wagner mechanism

At the MgO/spinel border, disseminated 2Al³⁺ reacts with MgO to generate MgAl₂O₄, whereas at the Al₂O₃/spinel barrier, diffused 3Mg²⁺ reacts with 3Al₂O₃ to form 3MgAl₂O₄. As a result, two MAS layers generated on the alumina side to magnesia side have a thickness ratio of 3:1. If the Wagner mechanism is absolute, the thickness ratio of two MAS layers generated on the Al₂O₃ and MgO sides, represented by R, is always 3. However, due to differences in composition and sintering temperature, this R value was found to be higher in real experiments. $R = \frac{3(7n+1)}{(3n+5)}$ was stated as the R value for the composition MgO·nAl₂O₃. Within the 1495–1595°C temperature range, R values are found to range from 4.1 to 4.6. It doesn't matter if the specimen is single or polycrystalline. The vapour movement of MgO is the other metric. At 1527°C, the saturation vapour pressures of MgO gas in the

presence of periclase and MAS are 2.5 and 6.2 Pascal, respectively. These findings suggest that MgO molecules evaporated by periclase may sink to the corundum surface to form MAS. If the contact between magnesia and alumina is rough, MgO vapour diffuses through the gap and subsequently forms MAS solely on the alumina side, resulting in an increase in R value. A diffusion couple in rough contact was found to have a value of R is 5.6 at 1535°C. R becomes infinite if MgO diffuses only in one direction to the alumina side. In reality, in a powder compact, there are three types of particle contacts: Al₂O₃–MgO, Al₂O₃–Al₂O₃, and MgO–MgO pairs. A stoichiometric MAS is obtained when the molar ratio of alumina and magnesia is 1:1.

On the MgO side, four MgO transform to one MgAl₂O₄ in the MAS production based on Wagner process. This region has a volume change of 0.884. Four Al₂O₃ change to 3MgAl₂O₄ on the Al₂O₃ side, with a volume change of 1.167. As the MAS formation progresses, the MgO side shrinks and the Al₂O₃ side expands. Alumina and magnesia have a molar volume ratio of approximately 7:3. Magnesia part reduces to 0.271 after MAS production.

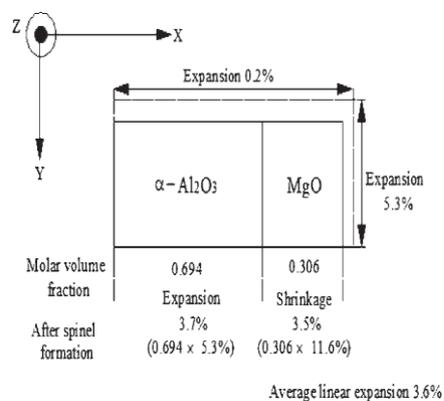


Figure 2: Expansion model of two particles system of alumina and magnesia

On an analogous direction, the alumina part expands to 0.731. The total is 1.002, which is a 0.2% linear enlargement. The Y and hence the Z expansions are 5.3% as the corundum part expands isotopically, and an increase in R will increase the enlargement of the Al₂O₃ aspect. The corundum section of R has a linear enlargement of over 100%. Navias [18] conducted an interesting experiment in which a piece of sapphire was individually placed from MgO and cooked in a

1900°C environment. According to the formation of MAS, the initial corundum gains a volume increase of 4.7%. This could be due to a MgO deficit.

In other words, once MAS is formed, the solid solubility of corundum, as well as the typical linear growth of the Al₂O₃–MgO mixture, is 3.6%. The typical enlargement is determined to be 4.1% once R is infinite. MAS formed at the interface of MgO and Al₂O₃ grains often isolates the reacting species, lengthening the diffusion channel and thus speeding up the reaction. This reaction is hastened in industry by carrying it out in two steps. The reactants are fired at a temperature of roughly 1200–1400°C in the initial stage for partial spinelization, followed by regrinding, re-compaction, and a second firing at 1700°C. Regrinding was discovered to be effective in transferring the reactive surfaces, which is required for a faster reaction.

The compact density, oxidation temperature, rates of heating and cooling, holding time at final oxidation temperature, and other characteristics of the raw materials, such as wet (both adsorbed/chemisorbed and hydroxyl radical groups), impurities (CaO, Na₂O, etc.), average particle size, particle size distribution, and compact density, were all found to affect the MAS section formation. At 1300°C, a compacted mixture of aluminum atomic number metallic element metal and metal hydroxides reacted to create MAS section in one hour, whereas a uniformly compacted mixture of metallic element and metal oxides required four hours of holding time to achieve an equivalent quantity of MAS section. The chemical compound precursors react at a slower pace than their comparable hydroxide precursor mixes, according to these research.

Furthermore, it is generally agreed that the MAS section formation temperature function should be unbroken as low as possible to avoid the creation of numerous agglomerates, which would otherwise catch the sintering activity throughout the compression operation. To reduce the process temperature and price of dense MAS grains for refractory applications, the effect of raw materials sorting and composition on MAS production and compression behaviour in a single-stage fire method was thoroughly explored.

In a study, Tripathi et al.[19] observed the result of MgO reactivity on formation and compression

behavior of MAS in a single stage reaction firing method at 1650–1750°C for two hours. The mixture of calcined corundum and gently calcined (1100°C) reactive caustic MgO or inert forge MgO was used in the process. The volumetrically enlargement information related to MAS section formation was employed to spot the initial MAS sintering temperature by dilatometry. The section formation from a mix of reactive caustic MgO and corundum mixture was found to be on top of that of the opposite. So, this can be said that the reactive caustic MgO had a better extent and lower crystal size. It is impressive to notice that, though the mixture of caustic MgO and corundum shows quicker section formation, their compression rate was set to be lower compared to the opposite one. The upper volume enlargement and grain growth related to the improved section formation was found to be liable for the noted inferior sintering behavior.

In another study, Sarkar et al. [20] discussed the outcome of corundum stuff content (i.e., non-stoichiometry) on compression behavior of reaction forge MAS at 1600–1700°C for 2 hours. The corundum made MAS developed an inferior forge property compared to those developed by magnesium oxide made MAS. During this case, the grain growth suppression was noted due to excess MgO at grain boundaries. Moreover, the corundum made composition developed comparatively big size grains. Yet, the degree of compression levels achieved for these MAS grains prepared in a very single step reaction sintering route are not sufficient for many refractory applications.

Mineralizes are utilized to accelerate the section formation and compression of MAS. One style of mineralizes reduces the mineral forming temperature and therefore the different sort reduces the sintering temperature. The AlF_3 , V_2O_3 and MgCl_2 fall within the initial class, whereas TiO_2 , Y_2O_3 , LiF , B_2O_3 , ZnO , Fe_2O_3 and CaO belong to the second class. The atomic number 5 containing compounds have been found which shows success as mineralizes for MAS formation. However, >2 wt.% B_2O_3 resulted the formation of $\text{Mg}_3\text{B}_2\text{O}_6$ crystals, that have turned the specified mineralizing result throughout MAS section formation. Due to high viscousness, this MgO changed boro-aluminate liquid shows little or no fluxing result. Moreover, its wettability was observed to be terribly low towards corundum and magnesium oxide grains. Besides, $\text{Li}_2\text{B}_4\text{O}_7$ and $\text{Na}_2\text{B}_4\text{O}_7$ were

found to be terribly effective fluxing agents and increased the reaction rate of MAS section formation by reducing the viscousness of soften and by increasing the wet ability. In another study, synthesized MAS powder by heating a one mole composition of MgO [21] and Al_2O_3 in LiCl , KCl or NaCl . A decrease within the MAS section formation temperature was noted from 1300 to 1100°C in LiCl , and 1300 to 1150°C in KCl or NaCl . The MAS powder produced during this method was established to be in pseudo morphic and preserved, to an outsized extent, the scale and morphology of the first Al_2O_3 stuff.

This means that a templet formation mechanism is important during this method. Moreover, apart from salts of Mg and Al based, all different mineralizers practically contaminate the MAS product and reduce its applications to lower temperatures only. One stage firing method known as electrofusion technique is additionally utilized to prepare high purity MAS. In the process of this method, the mixture of calcined corundum and natural mineral is molted in an electrical arc furnace. Temperature generated in this method volatilizes impurities. Hence, this method is of energy intensive and not stable to apply by several of the countries where electricity is expensive for several of the refractory applications. In another different single stage firing method, Sarkar et al.[22] produced dense MAS grains with a theoretical density (TD) of 99.5% at 1600°C. In this method, edge was used for six hours to cut back the particle size of beginning raw materials mixtures. Nevertheless, in this method, there's a prospect that grinding media used for erosion of edge contaminate in MAS grains.

To spot a lot of economic routes for synthesis of MAS powders via solid state reaction in refractory applications, the microwave (MW) energy was considered in a very recent study, Ganesh et al. [23]observed MAS powders affected by metallic element and metal oxides as beginning materials in a very domestic microwave kitchen appliance. For comparison, an equivalent raw materials mixture compact was calcined in a very standard electrically heated chamber at 1350°C for 1 hours to get MAS powder with ninety-three mineral section. Time consumed during this latter standard method was 24 hours. Moreover, once an equivalent raw materials mixture compact was treated in an microwave kitchen appliance with the assistance of elemental

carbon, a substantial quantity of MAS section formation was found at an interval of 60 minutes. The XRD spectroscopy of MAS powders obtained in microwave kitchen appliance with the assistance of various amounts of carbon. It will be seen that even twenty World Trade Center carbon is sufficient to convert raw materials mixture into eighty-two MAS section. These XRD results clearly reveal that the MAS powder will be synthesized at a lot of lower time intervals and with a minimum current input in a microwave kitchen appliance by utilizing the chemically potential of raw materials compared to the standard oxidization route in an electrical chamber.

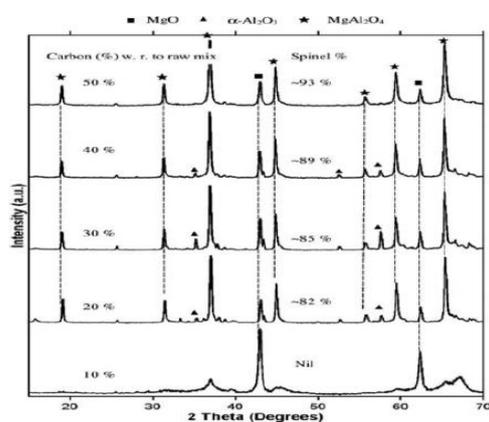


Figure 3: X-ray diffraction patterns of MW treated stoichiometric mixture of Aluminium tri hydroxide and caustic MgO in presence of different amounts of carbon

Yet, the carbon source is a limitation here to practice this process in industry. Mechanochemical synthesis (MS)/mechanical alloying (MA) is also tried to produce MAS powder through solid state reaction to bring down the powder synthesis costs. In a study, Mackenzie et al [24] synthesized MAS precursors by MS/MA exploitation $\text{Al}(\text{OH})_3$ and $\text{Mg}(\text{OH})_2$ or basic metallic element carbonate as raw materials. It is observed that heating of resultant precursors at 850°C produces MAS powders. The MAS powder derived from the hydro mineral containing precursor showed good sintering ability at $1400\text{--}1600^\circ\text{C}$, producing a mould body of 97 TD at 1600°C . With the similar atmosphere, the brucite derived MAS achieved 72 TD and showed amorphous property consisting of large grain sizes.

In another study, Kim and Saito [25] observed that MAS powder can be produced by combination of $\text{Mg}(\text{OH})_2$ and mineral followed by calcining at 800°C .

Although MS/MA may activate the solid-state reaction at temperature, the treatment at 800°C was required.

In another study, Kong et al. [26] synthesized MAS powder with a average grain size of 100 nm at 900°C from a combination of MgO and Al_2O_3 high energy processed for twelve hours. The operation was carried out in a planetary ball mill in air at room temperature. These powder crystals became dense MAS ceramics with 98 TD with an AGS (average grain size) of 2 to 5 millimeter upon sintering at 1550°C for two hours.

However in another study, Lavat et al. [27] produced MAS powders from $\text{Al}_2\text{O}_3\text{--MgO}$, $\text{Al}(\text{OH})_3\text{--MgO}$ and $\text{Al}_2\text{O}_3\text{--MgO}$ mixtures at room temperature in air atmosphere following MS/MA route. The formation of MAS occurred quicker with Al_2O_3 than with $\text{Al}(\text{OH})_3$ when one hundred forty hours, in MS/MA method, the mixture of $\text{Al}_2\text{O}_3\text{--MgO}$ crystal converted to the formation of MAS with ninety-nine section.

In another study, Kuntz et al. [28] plotted the reaction bonding method for MAS ceramics that shows negligible shrinkage throughout sintering and possess high gas tightness in spite of residual consistency. In standard fabrication routes, this methodology utilizes atomic number 13 metal and magnesia as precursors. Al or Al-Mg alloys used for this purpose had low melting points near to 660°C . The precursor mixture produced in the edge of reaction mixture was reproduced into MAS section at 1400°C . The MAS yield was established to be lean on the initial particle size of raw materials and therefore the diffusion lengths between reacting species.

Yet, in another different study, Henkel et al. [29] synthesized MAS powder by high energy ball edge of MgO and antimonial Al-3 wt.% Mg followed by oxidation at 1400°C . Results noted during this study were almost like those noted by Kuntz et al. [28] Nonetheless in another study, Tian J et al. [30] studied the result of high energy edge on the decomposition behavior of precursors shaped by the sol-gel route and on the formation behavior of MAS section. The procedure decreased the American state hydroxylation temperature of $\text{Al}(\text{OH})_3$ from 190 to 130°C . The energy of activation for MAS formation was decreased from $688\text{ kJ}\cdot\text{mol}^{-1}$ for readymade precursors to $468\text{ kJ}\cdot\text{mol}^{-1}$ for the precursors processed for five hours. Edge of the precursor mixture downgrades the temperature of MAS

formation from 900 to 800°C. Therefore the temperature of complete MAS spinel formation changes from 1280 to 900°C. The energy of activation of those reactions has been calculated following the process developed by Henry Alfred Kissinger[31] Krylova and Stevulova [32] studied the dynamics of solid-state reaction of MAS formation throughout MS/MA and confirmed it.

In another study, Kumar and Sundhage[33] studied the fabrication of close to web formed MAS bodies within the sort of discs and bars by infiltration of liquified metallic element into porous aluminum oxide. A bulk density (BD) of 3.34 g.cm⁻³ (92.7% TD) was observed with a lowest dimensional variation, sintered at 1700°C for six hours. Since, antimonial Mg₂[metallic element metal] is costlier and far lighter (1.74 g.cm⁻³ versus a pair of 0.70 g/cm⁻³) than atomic number 13, this method has been studied to be not viable to follow commercially. Also, the total heat of fusion of Mg (2.14 kcal.mol⁻¹) is slightly below that of Al (2.58 kcal.mol⁻¹). Hence, for increased penetration of the liquid metal into associate degree compound matrix, and for favourable thermodynamical and kinetic aspects is associated with the economy of the method.

Considering these advantages, Ping et al.[34] used antimonial atomic number 13 rather than metallic element with MgO to synthesize MAS powder through self-heat sustained (SHS) route within gentle reaction conditions. vasoconstrictor melting of atomic number 13 and resulting chemical reaction between liquified atomic number 13 and periclase perceived to have crystal rectifier to a powder with a awfully high fraction of the MAS section with tiny particle size and slim particle size distribution. This powder upon sintering for four hours at 1600°C has shown compactness with density as high as 92 TD.

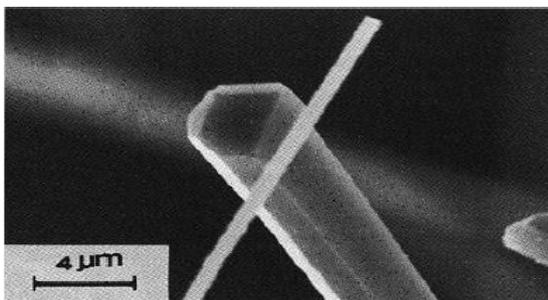


Figure 4:Image (SEM) of MAS whisker grown by heating at 1500°C for 4 hours.

In another investigation, Hashimoto and

Yamaguchi[35] produced MAS whiskers with a diameter of 3.10 millimetre and a length of 4.0 millimetre from a mixture of MgO, C, and Al heat treated at 1500°C for 8 hours in a carbon monoxide and greenhouse emission atmosphere. This reaction took place when the reactants were oxidised and reduced. On plane (111), the whiskers were fully developed. The partial pressure of oxygen required for MAS whisker formation was determined to be between 10-12.10 and 10-11.5 MPa. MAS whiskers are typically produced by a vapour section reaction.

In a separate work, Wolf associate degreeed Coskren[36] produced MAS whiskers by heating a powder mixture of MgO and Carbon in an Al₂O₃ tube with an inert gas flow at 1550°C.

Suvorov et al. [37] investigated the expansion of MAS whiskers by burning MgO associate degreeed Al₂O₃ rods in an Al₂O₃ tube covered with a carbon lid at temperatures ranging from 1300°C to 1800°C.

In a separate investigation, Xanthopoulou[38] used the self-propagating heat synthesis (SHS) method to make a MAS powder. Powder mixes of MgO, Al, and Co₃O₄ (as a dopant to reinforce the chemical activity), and in rare circumstances, Al₂O₃, MgO, or SiO₂ were used as the starting charges. Cylindrical samples were generated by uniaxial compaction at a pressure of up to 20 MPa after mixing the original parts in air. In a heating chamber, these compacts were processed at 770°–920°C. A small amount of thermite mixture was used to start the SHS combustion (85 percent Fe₃O₄ and Al). Because of the high combustion temperatures attained by SHS (1.2–1.8 m₂.g⁻¹), the powder produced by this process has a reasonable compressive strength (5–6.5 MPa) and a small area. The MAS powders produced via solid state reaction synthesis techniques aren't suitable for making optically transparent ceramic windows, domes, or armour

Soft resolution chemistry routes:

The powders made in soft resolution chemistry routes are most popular for certain applications, such as optically clear windows/domes/armours, catalysts and catalyst supports, humidity sensors, and so on, due to their superior powder characteristics when compared to those made in the solid-state reaction routes described in the previous sections. Soft resolution chemistry routes offer a number of advantages, including the ability to control product homogeneity and purity, the size, shape, and

distribution of the resulting ceramic particles, and process temperatures, all of which are becoming increasingly important in the manufacture of advanced ceramic products. [39], [40]. In an exceedingly study, Bratton[41]–[43] ready MAS powder by calcining a compacted ratio mixture of aluminum hydroxide and cathartic. This powder upon compaction and sintering at 1600°C for 6hr discovered a density such as 96 TD (Theoretical Density).

In another study, [44]hydrolyzed a mix resolution of metal and aluminum nitrates exploitation carbamide as a hydrolyzing agent at 900°C to get a mix of gel-like amorphous corundom hydrate and $Mg_4Al_2(OH)_{14} \cdot 3H_2O$ phases. This mixture diode to a dense MAS body with 99 TD upon sintering at 1600°C for 4 hours. Another work used ammonia carbonate as a hydrolyzing agent to produce a MAS precursor mixture consisting of crystalline ammonia dawsonite hydrate ($NH_4Al(OH)_2CO_3 \cdot H_2O$) and hydrotalcite ($Mg_6Al_2(CO_3)(OH)_{16} \cdot 4H_2O$) phases. This precursor forms a transparent MAS body after being oxidised at 1100°C for 2 hours, regrinding, recompaction, and a second firing under vacuum at 1750°C for 2 hours with no sintering additives.

Zawrah et al.[45] generated a crystalline MAS powder using metal and aluminium chlorides as precursors at 1000°C in another investigation. Die ironed compacts of this powder exhibited. and 96 TD when sintering at 1550°C with 2 wt. percent ZnO or 3 wt. percent MnO_2 as sintering aids. When compared to the doped samples from the International Organization, these samples had better mechanical properties. J li et al. [46]used carbonate as a causative agent to precipitate Mg and Al nitrate precursors, resulting in the synthesis of $NH_4Al(OH)_2CO_3 \cdot H_2O$. (ammonium-dawsonite).

This ammonium-dawsonite was reborn as hydrotalcite, $Mg_6Al_2(CO_3)(OH)_{16} \cdot 4H_2O$, after age. Because each of those phases was in such close proximity, it was easier for them to decompose into crystalline MAS powder. These powders were discovered to be ideal for producing transparent MAS parts. Rashad et al. [47] manufactured one-section nano crystalline MAS powder from anhydrous aluminium chlorides and metal using either characin fish alkyl liquid as a precipitant or 8-hydroxylquinoline as a complexing agent in another investigation.

When oxidised at 600°C, the MAS powder made with 8-hydroxylquinoline had a specific area of 182 $M_2.g^{-1}$ with tiny rod-like structures, whereas the one made with characin fish alkyl liquid had spherical generated particles when hardened at 1000°C. Schreyeck et al. [48] produced MAS powder by heating a combination of magnesium and aluminium sulphates at 1200–1600°C for 2–14 hours. A nonconductor was observed in the MAS powder that had been fashioned at 1600°C for 14 hours. However, powders made via coprecipitation processes using metal chlorides, sulphates, nitrates, carbonates, and other precursors always contain some residual anions as impurities, which are difficult to remove. When these ion contaminants occupy grain boundaries during sintering, they cause dispersion of transmitting lightweight, giving the forge bodies a translucent appearance.

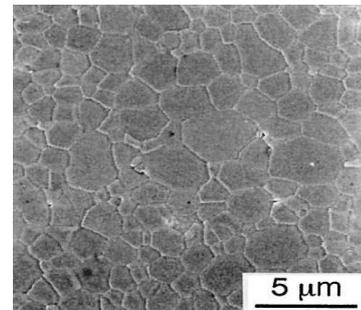


Figure 5: Image of SEM microstructure of MAS sintered at 1500°C for 3 hours The MAS powders.

Without any such ion impurities, the sol-gel technique, which uses high purity alkoxides as precursors, can be used to prepare them.

C Mathew et al.[49] used a sol-gel method to produce a high purity ratio MAS powder using metal iso propoxide and atomic number 12 nitrate as precursors. Yuan et al.[50] prepared MAS powder using a modified sol-gel technique that used nitrates instead of alkoxides as precursors and Xanthan gum and locust pod gum as gel forming agents. After oxidation at 800°C, the gels fashioned using this process crystallise into a nm-sized MAS powder with a median crystal size of twenty nm. In a separate work, Ye et al. [51] prepared MAS powder using a sol-gel seminal fluid precipitation method with metal iso propoxide and atomic number 12 acetate as starting ingredients. After oxidation at 900°C, the gel fashioned by this process crystallises into a totally crystalline ratio MAS powder.

K. Patil et al.[52] used a heterogeneous alkoxide resolution with terribly fine MgO powders to manufacture a terribly fine, with chemicals ratio, high purity, and extremely reactive MAS powder by sol-gel technique. The powder was compacted to a totally dense microstructure at 1200°C for 1 command under fluid dynamics pressure of 350 MPa, then sintered at 1500°C for 3 hours without the use of any sintering additive. Despite the fact that the sol-gel approach creates single/composite chemical compound powders with regulated textural and surface qualities, the atomic homogeneity of the powders produced by this method is poor. By selecting alternate alkoxide precursor materials, concerns linked to the creation of atomically homogenized binary chemical compound materials by the sol-gel method will be resolved due to the varied reaction and condensation rates of various metal cations. By allowing pre-reaction with water, a less reactive precursor will gain an advantage. This approach, known as 'Prehydrolysis,' is the most commonly employed reactivity matching motif in sol-gel synthesis.

A highly reactive precursor, on the other hand, will be over-involved if a number of its alkoxy teams are commutated with completely different ligands during a process known as 'chemical modification.' Ethanoic acid and acetyl radical solvent are two of the most commonly used chemical modifiers. Due to the use of costly alkoxide precursors, MAS powders made by sol-gel methods are generally high-priced, and thus are only suitable for constructing high-end items like optically clear aromours/windows/domes. Recently, combustion synthesis has emerged as a suitable powder synthesis technique that is both simple and cost-effective[53].

This approach eliminates the need for acids and bases to hydrolyze the relevant salts, as well as laundering, filtering, drying, and oxidisation procedures, saving a significant amount of energy and time. These powders, on the other hand, are less sinterable due to their smaller surface areas and plate-like powder morphology. The amount of gases that escape during combustion is mostly determined by the type of fuel used and the amount of fuel consumed (i.e., the upper the molecular size and weight of the fuel the larger the gas generation). Because the separation of the fuel molecule increases the distance between two neighbouring

metal ions within the resolution, the contact of the hydrolyzed metal ions can diminish, resulting in fine particles. As a result of these advantages, the solution combustion synthesis is also used to make MAS powders using several types of organic fuels, either in a traditional electrical kitchen appliance or in a MW kitchen appliance.

Bhaduri et al. [53], [54] created nanocrystalline ratio MAS powder using metal nitrates as oxidizers and organic compounds as a fuel in a study. The powder formed by this approach was solidified using the slip casting route, followed by ten minutes of cold isostatic pressing (cipping) at 275 MPa. As a result, the resultant compact was hot isostatic ironed (hipped) for four hours at 1300°C to produce a dense MAS body with a hardness of 779 weight unit.mm-2. Ganesha et al. [55], [56] produced MAS powders using plant products and organic compounds as fuels in another investigation. The powder made from organic compounds had a median particle size that was many times greater than the one made from a plant product combustion approach. The plant product-derived powder had a Breunauer Emmett and Teller (BET) extent of 65.8 m².g-1, whereas the organic compound-derived powder had only 8.06 m².g-1 due to its fine particle size. Furthermore, after sintering at 1625°C for two hours, the plant product derived powder was densified to a bachelor's degree of three.44 g.cm-3, an apparent body (AP) of one.76 percent, and a water absorption capability (WA) of zero.52 percent, whereas the organic compound derived powder had a much lower bachelor's degree after sintering under identical conditions (3.24 g.cm-3).

Due to the low sintering ability of organic compound combustion produced powders, Bhaduri et al. used the hipping technique to densify organic compound combustion derived MAS powders. To reduce the particle size of organic compound combustion generated MAS powders, Ganesh et al. [57], [58] used a commercially available home MW kitchen appliance operating at two.45 gigacycle frequency to conduct combustion synthesis tests. During a MW kitchen appliance, the batch size had a greater impact on the characteristics of combustion produced powders. Once the batch size was inflated from two to a hundred g, the surface areas of powders bated from 36.8 to 0.1 m². g-1 for MW synthesised powders and from 126 to 8.1 m².g-1 for common electrical kitchen appliance manufactured powders. This could be due to the sample sintering

due to the high adiabatic temperature generated as a result of increased heat accumulation with larger particles. The grains/crystals in the MW and standard electrical kitchen appliance powders had average diameters of 20–50 nm and 100–250 nm, respectively.

In a separate investigation, produced MAS powder by using metal nitrates as oxidizers and organic compounds such glycine and b-alanine as fuels in a combustion pathway. Organic substance was shown to be the best fuel for metal nitrate, whereas b-alanine was found to be the best for atomic number 12 nitrate. The simplest findings were obtained using merely a mixture of fuels (urea and b-alanine, organic molecule, and glycine) in the case of MAS. The use of fuel combinations allowed for the direct creation of pure, nanocrystalline MAS from the combustion reaction, without the need for a subsequent tempering step. the use of a single fuel (urea, glycine, or b-alanine) crystal rectifier to the creation of an amorphous powder that required tempering to achieve crystalline MAS.

Pacurariu et al. [59] synthesised MAS powder utilising a resolution combustion method with a consistent set of organic fuels (urea, glycine, and b-alanine) and compared the powders' properties to those of powders synthesised using organic precursors using a sol-gel technique. The size of the crystal is influenced by the type of fuel used. The powder made from the combustion of organic compounds had a median crystal size of 3.45 nm, 8.34 nm for the powder made from the oxidation of metal and atomic number 12 glyoxylate combination, and 10.36 nm for the powder made from the combustion of b-alanine at 700°C. In another study, Alinejad et al. [60] used metal nitrates and a complex matrix precursor made of plant product and polyvinyl alcohol to make nanocrystalline MAS powder. According to an XRD examination of those powders, the MAS component synthesis temperature for this technique was between 600 and 700°C. The crystal size ranged from 8–12 nm in the faceted formed morphology of the powder fashioned at 800°C for two hours. Furthermore, the quantitative link between the compound matrix and metal ions influenced the MAS powder crystal size significantly.

Polyvinyl alcohol was combined with ratio mixed metal nitrate resolution by Adak et al. [61] to develop a MAS precursor combination. The resultant precursor was processed into a completely crystalline MAS powder after oxidation at 800°C. Li et al.[62]

used a new mixture of gel-producing organic monomers to avoid the segregation of metal ions hydrolyzed from atomic number 12 and metal nitrates. A solution containing these organic monomers, metal nitrates, and organic molecules was regenerate into a gel with the help of a chemical change leader (i.e., ammonia persulphate at 600°C). After drying and oxidation at 700°C, the mixed Mg–Al hydroxide precipitates in a tiny space within the three-dimensional housing network fashioned within the gel, which junction rectifiers to fine nanoscale sized MAS particles. This method of resolution combustion synthesis has proven to be quite useful, especially for composite compound powders rather than single component powders. When compared to identical composite powders created using a very traditional solid state reaction approach and ratio MAS powder shaped using a combustion route, combustion synthesised ZrO₂–MgAl₂O₄ composite powders showed much improved shape and microstructure. As a process for producing chemical powders, hydrothermal synthesis has lately acquired prominence. The mixed Mg–Al hydroxide precipitates in a tiny region within the three-dimensional housing network fashioned within the gel after drying and oxidation at 700°C, which junction rectifiers to fine nanoscale sized MAS particles. This resolution combustion synthesis approach has proven to be quite beneficial, especially for composite compound powders as opposed to single component powders. When compared to similar ZrO₂–MgAl₂O₄ composite powders made using a fairly typical solid state reaction approach and ratio MAS powder formed using a combustion pathway, combustion synthesised ZrO₂–MgAl₂O₄ composite powders had significantly better shape and microstructure. Hydrothermal synthesis has recently gained popularity as a method for manufacturing chemical powders.

Higher microstructure management results in optimal and consistent characteristics of ceramics due to the reduction of aggregates mixed with slender particle size distributions within the starting powders. In light of these advantages, Z. Zeng et al.[63] used a hydrothermal approach to mix MAS particles in a study. MAS platelets with dimensions of 100–200 nm and a thickness of twenty-five nm were formed by hydrothermal treatment of AlO(OH) in a highly atomic number 12 nitrate solution at 400°C. In another study, Aminiet al. [66] prepared MAS powder using MgAl₂(OCH₂–CH₂OR)₈, dissolved in solvent,

using a hydrothermal motor-assisted sol-gel method.

The gels obtained from Mg-Al alkoxides contained 6 coordinated metal atoms in resolution, which junction rectifier to the formation of pure MAS part upon oxidization at 700°C, whereas the precursors of reagents three and four contained four coordinated metal and junction rectifier to the formation of MAS part in conjunction with some Al₂O₃ and MgO under similar reaction and oxidisation processes. Spherical particles are formed when processed in hydrophobic solvents, whereas non-spherical powders are shaped when processed in the parent alcohol. In terms of the loose baccalaureate of the resulting powders, the freeze drying process has recently been regarded to be preferable than the spray drying technique. The spray dried powder's skeleton is frequently a thin-walled hollow sphere, which results in the creation of pores within the shape samples, resulting in low baccalaureate.

Wang et al. [64] generated very sinterable MAS powder using alkoxide precursors and a freeze-drying technique in another investigation. The powder formed using this method had a shape density of >95% TD after cipping at 206.8 MPa and sintering for 3.5 hours at 1500°C. These MAS samples are formed by heating them to 1500°C in an Air environment at 200 MPa for 2 hours, resulting in a very transparent junction rectifier. Metal sulphates were utilised as the starting components in another investigation to assemble MAS powder using the same freeze-drying process. Vestal et al.

[65] generated MAS nanoparticles using a standard particle production technique in a study. A standard particle resolution was prepared at the start of this procedure by adding an associate solution of atomic number 11 dodecyl sulphate to an associate solution containing the required amounts of atomic number 12 nitrate and metal nitrate. The metal nitrates were hydrolyzed by dropwise addition of diluted liquid resolution at pH 10.3, grain alcohol was then injected into the suspension, and the flocculated particles were collected by activity during this particle resolution. The resulting material was processed at 800°C for 20 hours after drying at 100°C to produce completely crystalline MAS powder.

Meyer et al. [66] used a sol-gel sort reaction of alkoxides within the inverse micelles of water/oil tiny emulsions to make nano-sized MAS particles.

Mg[Al(O)4]₂, an affiliated hetero bimetallic alkoxide, was exploited as a source of MAS in this work. During this research, it was discovered that the detergent's hydrophilic chain length varied with the size of the water droplet, which had a significant impact on the resulting MAS powder particle size.

Furthermore, a single bimetallic precursor was found to be superior than combinations of two different metal alkoxide precursors in terms of supplying ratio MAS powder at significantly lower temperatures. Those shaped in soft resolution chemistry routes showed robust promise for process of advanced ceramic merchandise like optical clear domes/windows/armours and have a tendency to indicate higher performance as catalysts and catalyst supports due to their higher specific surface areas, smaller particle sizes, controlled crystal structures, and better purities when compared to powders shaped in solid state reaction synthesis routes.

Thick/thin films of MAS:

Thermal barrier coating (TBC) for the blades and vanes within the hot section parts of gas turbines, buffer layers for the expansion of compound superconductors, ferro-electric random access memory applications, wetness sensors, and electroluminescent phosphors are just a few of the applications for MAS thin/thick films. At first, MAS films will be prepared using physical vapour deposition methods such as sputtering, electromagnetic radiation evaporation, and other methods with inferior properties. However, numerous new processes, such as chemical vapour deposition (CVD), metal organic chemical vapour deposition (MOCVD), atomic layer deposition, plasma spray techniques, and others, have recently been developed to produce thick and thin films with a variety of improved properties. Conventionally fully developed MAS films from a reaction mixture of Al-HCl-MgCl₂-CO₂-H₂ at >1000°C, that junction rectifier to the development of CO and HCl as byproducts, were investigated in a comparable work.

The high reaction temperature, on the other hand, was the method's most serious flaw. The caustic and toxic byproducts formed through this process are also effective scaling deterrents. Metal organic chemical vapour deposition (MOCVD) has been established for similar functions to avoid these concerns. In one investigation, MAS thin films were produced at 850–950°C using a volatile chemical

agent motor-assisted MOCVD. Stollberg et al.[67] used combustion CVD to develop MAS thin films onto silicon oxide substrates and tested their performance as an over layer on TBCs used in the latest sections of gas turbines at temperatures ranging from 850 to 1150°C. Precursors employed in this work included atomic number 12, atomic number 12 dihydrate ($\text{Mg}(\text{C}_{11}\text{H}_{19}\text{O}_2)_2 \cdot 2\text{H}_2\text{O}$), and metal acetylacetonate.

The use of distinct sources for expanding MAS films, on the other hand, resulted in some deviations from ratio inside the films, leading in purpose defects and precipitates. Due of differences in lattice constants and thermal enlargement coefficients between MAS and Si, high growth temperature also resulted in significant tensile stress and lattice flaws inside the MAS films. In addition to the existing temperature constraint, CVD synthesis of MAS device architectures necessitates precision management of the atomic number 12 to metal quantitative relationship, as well as element content. Single bimetallic precursors are introduced to fully grown MAS films to overcome these drawbacks.

Recently, atomic number 12 di-metallic element isopropoxide, $\text{Mg}[\text{Al}(\text{O})_4]_2$, a bimetallic precursor with a constant 1:2 Mg/Al quantitative relationship, has been used to fully generate ratio MAS films at temperatures ranging from 500 to 1000°C. The structured thick MAS films are employed as electrolyte protection layers in solid oxide gas sensors.

Zhang et al. [68] employed $\text{Mg}[\text{Al}(\text{O})_4]_2$, a commercially available single atomic number 83 gilded precursor, to build crystalline crack free ratio MAS films on the surfaces of Si and MgO substrates at 400–600°C, following each thermal and plasma enhanced MOCVD. Over a wide range of deposition circumstances, the resulting films had the same Mg/Al quantitative relationship as the starting compound (Mg/Al 51: 2). Furthermore, when a remote plasma enhanced MOCVD approach was utilised, the deposition temperature required for the creation of crystalline MAS was found to be significantly reduced, and crystallinity on Si substrate was much improved. The MAS films formed on Si by plasma enhanced MOCVD at 700°C were epitaxial, with a breakdown voltage greater than 106 V cm^{-1} for 3 meter thick films, implying that MOCVD deposited MAS skinny films are useful for a variety of

electronic applications. F Meyer et al.[69] studied the chemical and material characteristics of MAS thin films shaped from three single molecular bimetallic precursors in the gas part, $[\text{MgAl}_2(\text{O}_2)_8]$, $[\text{MgAl}_2(\text{O}_2)_8]$, and $[\text{MgAl}_2(\text{O}_2)_4\text{H}_4]$. MA1, MA2, and MA3 are the several names for these precursors. The features of the MAS films formed from these precursors are a strong function of the precursor molecule's composition.

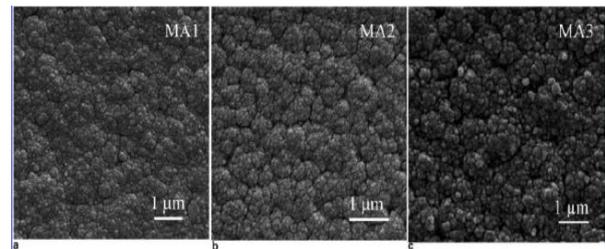


Figure 6: Image (SEM) of MAS films deposited on Fe at 550°C using a MA1, b MA2 and c MA3 respectively

The cross-sectional SEM photos of MAS films moulded on chemical element substrate from MA1, MA2 and MA3 are awarded in Figure. The SEM micrographs of MAS skinny films deposited on iron at 550°C using MA1, MA2 and MA3 are conferred in the above figure. The micrographs' options demonstrate that MAS skinny films produced from single molecular precursors are quite similar to those shaped using physical vapour deposition techniques. Rocheleau et al.[70] used the metal alkoxide supply, $\text{Mg}[\text{Al}(\text{O})_4]_2$, to produce amorphous skinny films of MAS onto crystalline chemical element and glass substrates at temperatures ranging from 250 to 500°C. The growth rate was found to be minimal at 250°C, but increased with substrate temperature between 300 and 425°C, indicating that the approach was surface reaction constrained.

The expansion was limited by the availability of chemical above 425°C, and no further increases in conversion potency or expansion rate were discovered. The alkoxide supply's volatility allowed for vaporisation at low supply temperatures, between 120 and 170°C. In fact, the alkoxide's fluidity at temperatures below 100°C allows for low-cost, high-rate spray transformation as a film deposition method. Putkonen et al. [71] developed MAS films on mixed glass and Si substrates by atomic layer deposition at 100–400°C using $(\text{C}_5\text{H}_5)_2\text{Mg}$, $(\text{CH}_3)_3\text{Al}$, and H_2O as precursors. The films originally deposited

were amorphous, whereas those treated at 800°C had a strong MAS structure. The pulsating quantitative relationship of the precursors was discovered to be important for film roughness. Were amorphous, but films annealed at 800°C had a MAS structure that was highly orientated. The pulsing ratio of the precursors was discovered to affect film roughness.

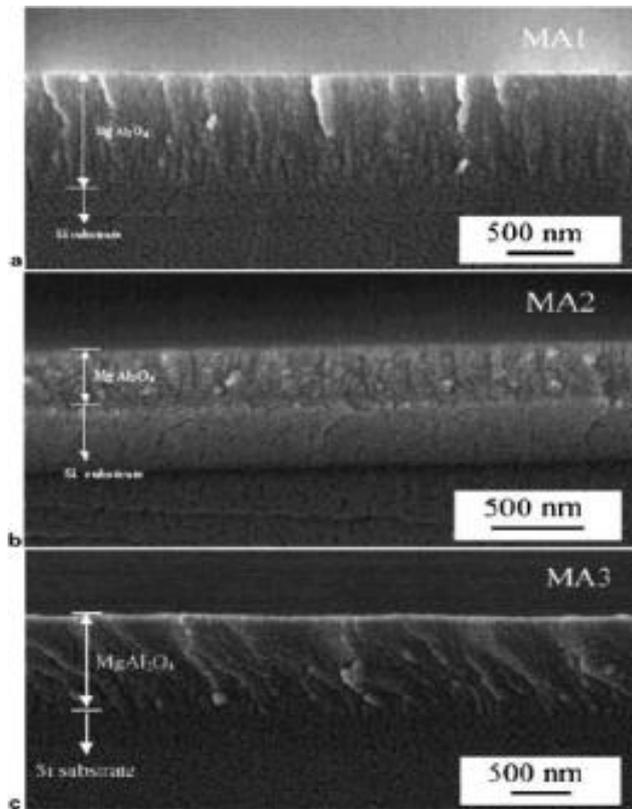


Figure 7: Cross-sectional SEM images of MAS films on silicon obtained from a (MA1), b (MA2) and c (MA3)

Plasma spraying is a rapid heating, cooling, and curing natural technique that always results in the development of deposits with a rough grain structure, vital body (usually between 8–15 vol.%), and lamellar morphology. Coarse powders (20–90 μm) are commonly used as feedstock materials in spraying procedures to create coarse structures. Bertrand et al. investigated the morphology and crystalline properties of MAS thin films produced using the dried particle plasma spray process, in which non-form spray dried particles were immediately injected into the plasma spray torch. Because it is backed by solid precursors, the dried particle plasma spray approach makes it possible to

build skinny structures with competitive deposition efficiencies in real time.

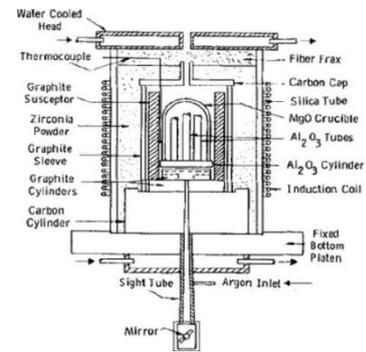


Figure 8 Apparatus for growing MAS single crystals

The form and chemical composition of the splats produced were undeniably dependent on the plasma properties (nature and power) as well as the powder injection parameters (carrier gas rate and spray angle). The initial oxides (MgO and Al₂O₃) react together to form MAS portion due to extremely thin mixing of the elementary powders. A roughness Ra of 3.8 μm was attained for a 200 μm thick coating by lowering the size of the starting particles. There were two sorts of splats identified.

The first is made up of individual well-thawed droplets, while the others are made up of nascent aggregates that have been thawed at their outside edges and simply reinforced in their centres. In Associate in Nursing plasma, the former was dominating, with semiconductor diode to dense coatings engineered of 1.0 μm thick splats, whereas the latter was prominent in Associate in Nursing plasma, with semiconductor diode to porous coatings. These discussions conclude that MOCVD of bimetallic single precursors may be better options for fabricating dependable MAS thin films for a variety of applications.

Fibres and single crystals synthesis:

MAS fibres and single crystals, in addition to skinny films, are unquestionably required applications. Mineral single crystals of MgAl₂O₄ are widely employed in bulk wave and MW devices, as well as fast IC epitaxial substrates. MAS has also been discovered to be a viable substrate for III–V compound devices. Liu et al.[72] created MAS fibres by transmuting extrudates made from a precursor recovered by vacuum evaporation of the solvent

from a 1:1 mixture of metallic element acetate and aluminium format soaked in water with stabilisers.

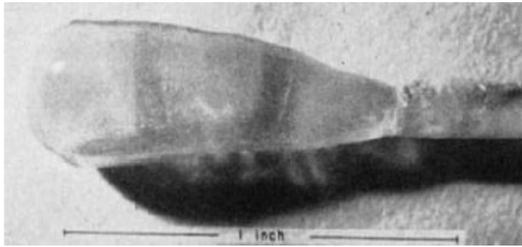


Figure 9 Single crystal boule of stoichiometric MAS grown by flame fusion with in situ annealing

With no solid indication of component separation, the MAS precursor behaved as a distinct compound and rotted to crystalline MAS immediately at 600°C. Furthermore, this MAS precursor may be easily extruded or drawn by hand to produce well-defined inexperienced fibres.

Bratton and Ho[73] used a custom designed chamber to fully develop MAS single crystals and fibres on aluminium oxide substrates. A forty-power unit Ajax-Northrup spark gap generator was used to heat this chamber. Only crystals were totally developed on the exterior wall of the MgO melting point at 1800°C in element atmosphere for 6 hours. The MAS crystals developed toward the MgO after being fashioned on the surfaces of an Al₂O₃ substrate. Fibers measured up to 25.0 millimetres in length and had diameters ranging from 7 to 8 millimetres. Up to 5.0 millimetres long, 0.2–1.2 millimetres wide, and 0.014–0.05 millimetres thick are examples of living matter measurements.

Many extremely thin platelets suitable for lepton transmission investigations are created. Arlett and Jerome Robbins totally grown one crystal decoration of ratio MAS by flame fusion technique (Verneuil process) at 1900°C, then treated in place from 1450 to 4000°C at 10°C.hour-1. [74] In this process, a porous cake was made by heating a mixture of 33.3% MgSO₄·7H₂O and 66.7% AlNH₄-(SO₄)₂·12H₂O to 400°C. This cake was crushed and calcined for 16 hours at 1200°C in a Globar chamber. The resulting powder was then filtered into mesh fractions ranging from -120 to +200 mesh and utilised as feed powder in the flame fusion chamber.

Using a multiple tube flame fusion burner heater for in-situ hardening, a MAS single crystal decoration is totally created out of this powder with and without

seeds. The heater was set at 1450°C, while the crystals were fully formed. The ornament was dropped into the new zone of the heater after the MAS crystal expanded. The gases were gradually cut off at this point, and the decoration was cooled to 400°C.

Sol-Gel & Precipitation (SGP) processes:

We have a tendency to gift a unique chemical method that integrates sol-gel and precipitation procedures, according to Guotian Ye, W patron saint Oprea, and Tom Troczynski [75]. This procedure begins with the hydrolysis of atomic number 13 isopropoxide [Al(-O-C₃H₇)₃] to form a solution, followed by the homogenous mixing of atomic number 12 acetate solution within the aluminium oxide sol. The pH is then increased to produce milk of magnesia precipitate at regular intervals in the aluminium oxide sol. In the sol-gel precipitation (SGP) method, homogenised intermixture of atomic number 12 and aluminum-bearing materials is expected to edge the synthesis of atomic number 12 compound mineral at a relatively low temperature. The starting materials for the SGP manufacturing method of the mineral precursor were atomic number 13 [Al(O-C₃H₇)₃] and atomic number 12 acetate hydrate [Mg(CH₃COO)₂·4H₂O]. Isopropoxide powder (atomic number 13) (0.10 mol) was dissolved in alcohol (3.0 mol) and refluxed for 2 hours. By stirring at room temperature, atomic number 12 acetate hydrate (0.05 mol) was dissolved in H₂O (1.05 mol) to generate a near-saturated solution and reduce the amount of water utilized. After that, value-added atomic number 12 acetate aqueous answer solution was added drop-by-drop to the atomic number 13 isopropoxide solution and refluxed for 3 hours. Atomic number 13 isopropoxide hydrolyzed to the sol portion at this point, whereas atomic number 12 remained in the solution.

To start the second step of the procedure (milk of magnesia precipitation at the same time as gelation of the hydroxide phase), liquid was slowly added to the solution while stirring, and the pH price was kept at 9.5–10 for 3 hours. The suspension was then dried at 60°C for 12 hours, treated in alcohol for 15 hours with zirconium oxide balls, dried again at 80°C for 12 hours, and finally dried at 110°C for 24 hours. After that, the precursor samples were calcined for 5 hours at 600 and 900°C. A portion of the calcined powder at 900°C was treated for 0.5 hour in alcohol with 100g zirconium oxide balls in a planetary. The

processed precursor was dried for 24 hours at 110°C. Mistreatment associated X-ray diffraction was used to determine the phases of the as-prepared precursor as well as the calcined samples. With a heating rate of 10°C/min below a flow of chemical element, the dehydration behaviour of the precursor was observed using mistreatment thermo quantitative analysis (TGA) and differential thermal analysis (DTA). Transmission microscopy was used to analyse the crystallisation size and shape of the calcined powder. Using X-ray diffraction data and Scherrer's equation, the apparent crystallisation size of the calcined powders was estimated.

The Brunauer–Emmett–Teller (BET) nitrogen-gas sorption technique was used to determine the specific expanse of the calcined powders. The calcined powder's equivalent average spherical particle size was computed using the specific expanse. Such a computed "particle size" is a speculative existence of the attribute between crystallites. An optical particle size analyser was used to determine the agglomeration size distribution of the powders. These agglomerates, which describe affiliation between many crystallites or particles, are several orders of magnitude larger than the "crystallites" or "particles". In general, such agglomerates are porous and easy to crush in order to reduce their size by grinding for calcination operations.

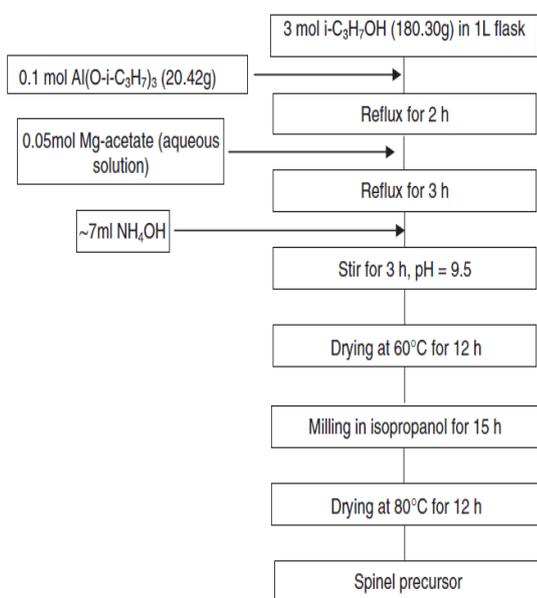


Figure 10 Procedures for preparing MgAl₂O₄ spinel precursor through the Sol-gel precipitation process.

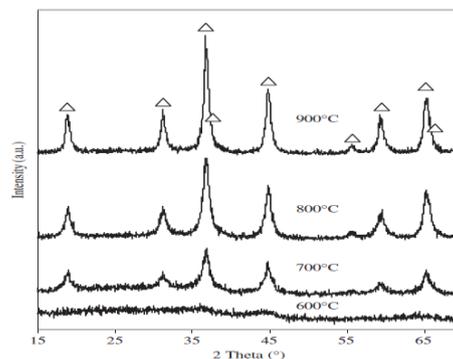


Figure 11 Spinel crystallization after 5 h of calcination at different temperatures.

At 600°C, the Al and atomic number 12 hydroxides in the precursor were completely dehydrated. As a result, the material remaining was likewise amorphous mineral, which started to form at 700°C and became phase-pure after fire at 900°C, which was much less than co precipitation (1100°C), freeze drying (1200°C), and heterogeneous sol-gel (above 1200°C). It is possible to believe that the oxidisation temperature is a crucial factor in powder agglomeration. As a result, the relatively low oxidisation temperature for section pure mineral production produced during this run via the innovative SGP approach is beneficial in preventing calcined powder aggregation.

Using an unique SGP approach, a spinel precursor was created. The separation of the steps of corundum sol synthesis from precipitation is a significant aspect of the technique (simultaneous with corundum sol gelation). A predisposition to assume that such a strategy improves precursor homogeneity, allowing the synthesis of phase-pure and even nano-particulate minerals at temperatures as low as 800–900°C. To reduce the tendency for particle agglomeration, alcohol was utilised as the dominating liquid medium in the precursor suspension. The apparent cry stallisation size, specific extent, and equivalent particle size of the calcined powder revealed soft agglomeration of the precursor after drying and also the powder after oxidisation at 900°C. As a result of the oxidation at 900°C followed by 0.5 hour. Edge ultrafine mineral powder (crystallisation size 28 nm) was formed.

Using this unique SGP process, phase-pure mineral was fashioned after the precursor was calcined at a relatively low temperature (900°C), proving that a uniform precursor was non inheritable. Because of

the moderate oxidation temperature, robust particle bonding and agglomeration of the powder would not occur after oxidation. The ideal temperature for producing mineral powder with high sintering reactivity would be within the range of 900°–1000°C, based on the relationship between specific surface areas, crystal size, and particle size and oxidation temperature. Larger/stronger agglomerates would be formed at temperatures of 1200°C or above.

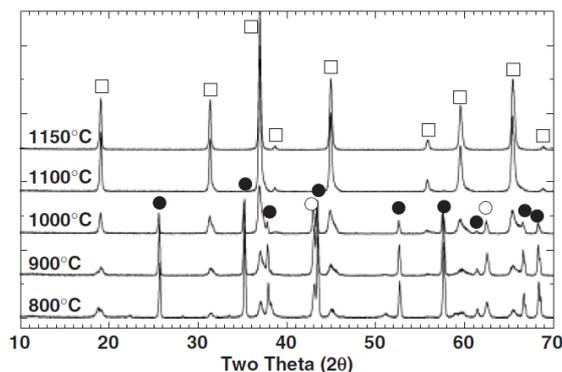


Figure 12 X-ray diffraction of spinel samples heated in LiCl for 3 hours at different temperatures

Molten Salt Synthesis (MSS) method:

Liquified salt synthesis (MSS), a low-temperature process, is gaining traction, it has so far been mostly employed to make comparatively low melting electro-ceramic powder. Associate degree exploration of MSS of MA powder is delineate to parenthetically the practicability of MSS for synthesis of high melting complex oxides. The main raw materials were calcined MgO and calcined Al₂O₃. KCl, LiCl and NaCl were utilised as salts.

Using a chalcedony mortar, an equimolar composition of MgO and Al₂O₃ was combined in the dissolver. The blended powder was then mixed with a variety of salts in a 55:1 salt/oxide weight ratio. The powder mixture was placed in a corundum tank with a corundum lid, heated to a temperature of 800°–1150°C, and then monitored for 3 hours. To remove the salts, the reacting mass was continuously rinsed with hot H₂O once the chamber reached temperature. Before further characterisation, the compound powders were oven-dried. For comparison, MA was also prepared using CMOS and the same heating schedules. Powder diffraction (XRD) analysis was used to determine the phases and extents of the reaction. Using Ni-filtered CuKα

radiation, spectra were collected at 30 mA and 40 potential units. MgO (45–946), Al₂O₃ (71–1123), and MA (75–1796) were the ICDD cards used for identification. To determine the impurity levels originating from the salt used, chemical analyses of the synthesised powders were performed using X-ray light (XRF) and inductively coupled plasma-atomic emission spectrum analysis (ICP-AES). Using an optical maser scattering technique, the particle size distributions of the raw materials as well as the synthesised MA powders were determined, as well as their microstructural morphologies.

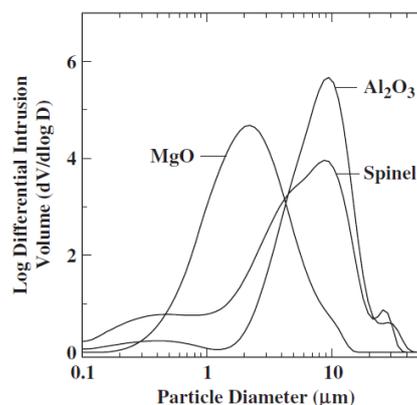


Figure 13 Particle size distributions of the Al₂O₃, MgO, and MA synthesized at 1150°C for 3 h in LiCl.

Spinel was not identified in CMOS samples after three hours at 900°C, whereas it had already started to type in LiCl after 3 hours at 800°C, showing that the MA formation temperature in LiCl is lower. Furthermore, one and five show that MSS was also successful in lowering the synthesis temperature at which pure MA was formed.

Pure MA was obtained in LiCl at 1100°C. However some Al₂O₃ remained in the sample when CMOS was employed at 1300°C, implying that the synthesis temperature of MA could be reduced by 200°C if MSS was used instead of CMOS. KCl and NaCl, like LiCl, increased MA development, though to a lesser extent than LiCl. However, a further examination reveals that the degree of reaction in two salts at 1150°C was similar to that in CMOS at 1300°C, implying that the synthesis temperature of MA may be reduced by 150°C if either of those 2 salts was used as a reaction medium. It's unclear why LiCl is more effective than KCl and NaCl at lowering the MA synthesis temperature, though one possible explanation is that MgO is more soluble in LiCl than

in KCl or NaCl. Processes, "dissolution–precipitation" and "template creation," are both involved in MSS. The merchandise part of the former occurs when the salt becomes oversaturated with reactants, whereas the additional soluble chemical dissolves in the salt, diffuses onto the surface of the insoluble or less soluble chemical, and then reacts to produce the merchandise that retains the insoluble or less soluble chemical's morphology and size. The particle size distributions of the synthesised MA were similar to those of the low solubility Al_2O_3 , and the MA retained the dimensions and shape of the Al_2O_3 to an enormous extent.

These findings suggested that the "template generation mechanism" is very significant in the MSS approach, however the "dissolution–precipitation mechanism" could not be completely discounted. MSS is used to manufacture MA mineral powders. The temperature of synthesis could be reduced from 300°C to 1100°C or even 1150°C . The synthesised MA kept the dimensions and shape of the original Al_2O_3 raw materials to an enormous extent, showing that the "template generation process" plays a critical role in the MSS approach.

Concluding Remarks

Because natural incidence is low, MAS is synthesised artificially and resides in an independent agency crystal structure. MgAl_2O_4 mineral has a high temperature (2135°C), high hardness (16 GPa), comparatively denseness ($3.58\text{gm}/\text{cm}^3$), high mechanical strength in space (135–216 MPa) and at elevated temperatures (120–205 MPa at 1300°C), high chemical resistance, wide energy band gap (0.7 eV), high electrical phenomenon, comparatively low thermal growth constant, high thermal shock resistance, and doesn't react with SiO_2 until 1735°C .

These features made MAS an essential and imperative material for applications such as clear windows, domes, and armours with wavelengths ranging from 2–5.5 metric linear unit, as well as refractory in cement rotary kilns' burning and transition zones, and steel ladles, among others. The effectiveness of MgAl_2O_4 mineral has also been tested in a variety of other applications, including thermonuclear reactor power core insulation, electronic moisture sensors, refractories, TBCs, catalysts, catalyst supports, and so on. However, a significant disadvantage of MAS may be the large amount of volume increase (8%) associated with the

production of its parts from corundum and periclase. During the latter method, MAS powder is first synthesised with 80% mineral content by calcining a compact mixture of corundum and periclase at 1400°C , and the resulting MAS powder is then ground to create recent reactive surfaces, and finally recompact to achieve a GD of a minimum of hour of the speculation.

This inexperienced body is then shaped at temperatures as low as 1700°C for long enough periods of time to get the appropriate density. The cost of production has been increased due to the use of two consecutive hot temperature firing cycles. This cost has been a real worry for refractory applications, which consume a larger amount of MAS's products. The process price of refractory grade MAS can be significantly reduced by using either a one-stage firing method, in which attrition milling is used to reduce the particle size of beginning (alumina and magnesia) raw materials to below one micrometre, or a two-stage firing method, in which precise management of optimised process parameters and extremely reactive beginning raw materials, as well as aluminium or metal primaril, is used.

If the introduction of contaminants into the final product from grain media is controlled, mechanical edge and MA procedures can significantly reduce the process cost of refractory grade MAS. Recently, the SAMH was shown to be a cost-effective and simple method for densifying MAS powders at much lower temperatures than previous methods.

At 1400°C , MAS does not want any susceptors to experience concentration because it has the required substance loss. As a result, MAS makes use of the MW activity generated in place throughout SAMH and achieves the necessary concentration at 1400°C . Even MAS component creation may be accomplished with this technology at significantly lower temperatures than with previous methods. As a result, there is potential for upgrading SAMH furnaces to synthesise powders, such as dense MAS grains, suitable for refractory applications at significantly lower production costs. Although the H.P. approach with LiF as a sintering aid has been shown to be successful in fabricating acceptable quality optically clear MAS elements, the cost of the procedure remains a concern. Given the wide range of critical applications of optically clear MAS ceramics in the strategic and personnel protection

sectors, as well as the higher performance of those MAS elements compared to their counterparts, such as corundum, sapphire, AlON, MgF₂, ZnS, and others, the reduction in process price will greatly improve the pertinence of MAS in many other trade sectors. The lower reactivity of the concerned starting powders, as well as the impurities present in them, have been linked to the use of difficult sintering conditions during HIPping, which has resulted in a large increase in the manufacturing cost.

As mentioned earlier in this critical review, many soft answer chemistry-based powder synthesis techniques, such as sol-gel, hydrothermal, freeze drying, traditional particle synthesis, and others, are capable of producing high purity and highly reactive MAS powders suitable for fabricating clear MAS ceramics with excellent optical properties under comparatively milder HIP or H.P. conditions. LiF and Y₂O₃ are well-known as excellent sintering additives for improving the concentration ability of MAS powder under milder HIPping conditions. LiF has also been found to be more effective at cleaning C and S impurities from MAS ceramics during HIPping operations, when they would otherwise cause MAS elements to expand by converting to gases.

Normally, C enters as an impurity into MAS clear bodies during SPS due to sputtering of black lead dies at high currents, rendering the sintered bodies opaque. Since LiF has been discovered to be successful in cleaning C from MAS ceramics, exceptionally clear MAS elements with a variety of improved optical properties will be developed in the SPS chamber by uniformly coating LiF on high purity nanosized MAS powder using a wet chemical impregnation process. The diameters of the black lead dies used in SPS furnaces, on the other hand, may be a constraint for producing enormous size elements. The assembly yields of transparent MAS ceramics for various necessary applications will be greatly enhanced if the diameters of the SPS chamber black lead dies are magnified and LiF is used as a sintering aid. A nano structured MAS densified with Y₂O₃ under comparatively milder HIPping conditions, on the other hand, exhibited an area temperature strength of 470 MPa, improved erosion resistance (sand and rain), and thermal shock resistance, as well as a near theoretical in-line IR transmission at RT, all of which are far higher properties than those normally exhibited by clear MAS ceramics shape without involving any sintering

additive. Certain sophisticated formed and large size MAS elements, however, cannot be invented using HIP or H.P. processes since they are too similar to web shaped components. Recently, a surface passivation technique for MAS powder was developed, allowing certain novel web form forming liquid colloidal processing techniques, such as GCHAS, gel casting, slip casting, and others, to be used to fabricate MAS domes at significantly lower producing prices, as high-priced and intensive post sintering machining operations utilising diamond tools will be completely minimised or eliminated. Using the MOCVD process, reliable and high-quality MAS thick/thin films may be made using single bimetallic organic precursors for a variety of applications, including TBCs. Flame fusion is a good way to make MAS fibres and single crystals, which are widely utilised in bulk wave and MW devices, as well as rapid IC epitaxial substrates.

Non-stoichiometry, as well as Frenkel or Schottky type defects, have a significant impact on the concentration behaviour of MAS powder. Excess periclase causes atomic number 8 vacancies to occur, which are known as rate crucial steps in the concentration procedure. Excess corundum, on the other hand, reduces the ability to densify to some level but greatly improves grain size, allowing them to perform better as a refractory in certain corrosive situations, such as the burning and transition zones of cement rotary kilns and steel abundant ladles. The Brouwer diagram, which was produced in theory, forecasts the creation of flaws and their type in MAS ceramics when excess periclase or corundum is inserted into the ratio MAS, proving the concentration ability of MAS powder.

Certain previously unknown properties of MAS dense bodies, such as Weibull modulus, thermal shock resistance, thermal physical phenomena, erosion behaviour against high speed sand and dirt, and also the photoluminescence, exposure emissivity, the degree of ion inversion, ratio, density of states, band gap energy, and so on, can be calculated using certain advanced characterization techniques. MAS's robust basic character, combined with its ability to withstand high temperatures and excellent abrasion and erosion resistance, made it a better catalyst and catalyst support for a variety of commercially important reactions, such as Sox abatement, CLC and CLR, NSR, dry gas reforming, and so on. Certain advanced soft answer chemical powder synthesis

processes, including as hydrothermal, conventional particle synthesis, sol-gel, and others, would provide nanosize powders with additional active sites in addition to the existing basic sites and the ability to endure high temperatures. As a result, nano-sized MAS powders are predicted to show a lot more promise for a variety of important reactions in the coming years, and they are expected to generate a lot of attention.

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Acknowledgements

The authors acknowledge TEQUIP II for funding